

Effect of Blade Friction on Performance of Micro-Hydro Pelton Turbines: Mathematical Modeling and Experimental Verification

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Department of Mechanical Engineering

University of Moratuwa

Sri Lanka

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Philosophy

Department of Mechanical Engineering

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July 2013

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ABSTRACT

Water turbines have been used in electricity generation for well over a century. Hydroelectricity now supplies 19% of world electricity and 44% (as at 2012) of Sri Lanka's electricity also comes from hydropower. Micro Hydro is a term used for hydroelectric power installations that typically produce up to 20 kW of power in Sri Lankan context. Many Micro-hydro power plants are operated with Pelton turbines. The main reasons for using Pelton turbines are that they are very simple and relatively cheap. As the stream flow varies, water flow to the turbine can be easily controlled by changing the number of nozzles or by using adjustable nozzles. Since most of the micro hydro Pelton turbines are now manufactured locally, it was revealed that much attention is not paid to the surface finish of the turbine buckets. On the other hand due to sand erosion of turbine parts bucket surface are getting rough day by day. Most of the research that had been done on turbines were focused on improving the performance with particular reference to turbine components such as shaft seals, speed increasers and bearings. There is not much information available on effects of blade/bucket friction on the performance of Pelton turbine. The main objective of this research is to analyze the performance of Micro hydro Pelton turbine particularly with respect to their blade friction.

The governing laws of fluid dynamics, relevant to the application were used to develop a theoretical model to estimate the effect of blade friction on Pelton turbine performance. Then the developed mathematical model was validated experimentally. All the experiments are carried out in a Pelton turbine standard test bench. The power developed by the turbine was measured by keeping all the relevant parameters that affect to the power development, constant other than the friction of the bucket. The friction of the buckets was varied by varying surface roughness of the buckets. Different roughnesses of the surface was obtained by pasting various grades of sands one at a time on the surface of the buckets

It was concluded from the developed mathematical model and the experimental testing that power developed by a Pelton turbine increases when the surface roughness of the turbine bucket decreases. It was also proved from the research that splitter thickness of the buckets is also affect the power developed by the turbine. When the thickness of the splitter increases power developed by the turbine decreases. Therefore it is recommended from the study that Pelton turbine buckets must be smooth as much as possible and splitter of the buckets should be as sharp as much as possible to generate more power from a power plant.

Key words: Pelton turbine, Bucket surface roughness, Splitter thickness

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TABLE OF CONTENT

| | |
|--|-----|
| ABSTRACT | iv |
| ACKNOWLEDGEMENT | v |
| TABLE OF CONTENT | vii |
| LIST OF FIGURES | ix |
| LIST OF TABLES | xii |
| NOTATION | xiv |
| CHAPTER 01: INTRODUCTION | 1 |
| CHAPTER 02: HYDRAULIC TURBINES | 5 |
| 2.1 HYDROPOWER MACHINERY | 5 |
| 2.2 HYDRAULIC TURBINES | 6 |
| 2.3 CLASSIFICATION OF TURBINES | 7 |
| 2.3.1 <i>The way of energy transfer</i> | 7 |
| 2.3.2 <i>Direction of Flow</i> | 7 |
| 2.3.3 <i>Position of Shaft</i> | 8 |
| 2.3.4 <i>Head utilized</i> | 8 |
| 2.3.5 <i>Installed capacity of the power plant</i> | 9 |
| 2.4 PERFORMANCE OF HYDRAULIC TURBINES | 10 |
| 2.5 THE SPECIFIC SPEED OF A TURBINE | 10 |
| 2.6 UNIT QUANTITIES | 11 |
| 2.7 EFFICIENCIES OF TURBINES | 12 |
| 2.8 CHARACTERISTIC CURVES OF A TURBINE | 12 |
| 2.9 CAVITATION | 17 |
| 2.10 SAND EROSION | 17 |
| CHAPTER 03: PELTON TURBINE | 18 |
| 3.1 INTRODUCTION | 18 |
| 3.2 THEORY OF PELTON TURBINE | 20 |
| 3.3 MAIN COMPONENTS OF A PELTON TURBINE..... | 21 |
| 3.3.1 <i>Runner</i> | 21 |
| 3.3.2 <i>Turbine shaft</i> | 22 |
| 3.3.3 <i>Turbine radial bearing</i> | 22 |
| 3.3.3 <i>Spear valve</i> | 23 |
| 3.3 PRINCIPLE HYDRAULIC LOSSES | 24 |
| 3.4 LOCAL SCENARIO | 28 |
| 3.5 RESEARCH NEEDS | 29 |
| CHAPTER 04: LITERATURE SURVEY | 32 |
| 4.1 INTRODUCTION | 32 |
| 4.2 ANALYTICAL STUDIES | 33 |
| 4.2 EXPERIMENTAL STUDIES | 33 |
| 4.2.1 <i>Flow observations</i> | 33 |
| 4.2.2 <i>Pressure measurements</i> | 34 |

| | | |
|---|---|------------|
| 4.2.3 | <i>Water film thickness measurements</i> | 35 |
| 4.3 | NUMERICAL MODELS | 36 |
| CHAPTER 5: MATHEMATICAL MODEL DEVELOPMENT | | 38 |
| 5.1 | CENTRIFUGAL FORCE | 38 |
| 5.2 | CORIOLIS FORCE | 40 |
| 5.3 | FRICTION FORCE | 41 |
| 5.4 | INFLUENCE OF SHAPE OF THE BUCKET | 44 |
| CHAPTER 6: EXPERIMENTAL FACILITIES AND METHODOLOGY | | 48 |
| 6.1 | EXPERIMENTAL FACILITIES | 48 |
| 6.1.1 | <i>Test rig</i> | 48 |
| 6.1.2 | <i>Sieve shaker and sieves</i> | 53 |
| 6.1.3 | <i>Surface roughness tester</i> | 54 |
| 6.1.4 | <i>Pneumatic grinder and grinder heads</i> | 55 |
| 6.2 | METHODOLOGY | 55 |
| 6.3 | BUCKET SURFACE PREPARATION | 56 |
| 6.4 | MAINTAINING A CONSTANT HEAD THROUGHOUT MEASUREMENTS | 59 |
| CHAPTER 07: RESULTS AND ANALYSIS | | 61 |
| 7.1 | RESULTS – EXPERIMENT NO 1 | 61 |
| 7.2 | EXPERIMENTAL DATA ANALYSIS OF EXPERIMENT NO 1 | 64 |
| 7.3 | THEORETICAL ANALYSIS | 76 |
| 7.4 | RESULTS OF EXPERIMENT NO 2 | 95 |
| 7.5 | EXPERIMENTAL DATA ANALYSIS OF EXPERIMENT NO 2 | 98 |
| 7.6 | THEORETICAL ANALYSIS OF DATA OF EXPERIMENT NO 2 | 107 |
| 7.7 | ANALYSIS OF EXPERIMENTAL DATA OF EXPERIMENT NO 1 WITH EXPERIMENT NO 2 | 118 |
| 7.8 | THEORETICAL ANALYSIS OF EFFECT OF THICKNESS OF SPLITTER | 126 |
| 7.8 | OTHER EFFECTS TO BE CONSIDERED | 134 |
| 7.8.1 | <i>Spillway effect</i> | 134 |
| 7.8.2 | <i>Mixing losses</i> | 135 |
| 7.8.3 | <i>Draining-off</i> | 135 |
| 7.8.4 | <i>Coanda effect</i> | 135 |
| 7.8.5 | <i>Jet boundary interaction</i> | 136 |
| CONCLUSION AND FURTHER RESEARCH | | 138 |
| 8.1 | CONCLUSION | 138 |
| 8.2 | RECOMMENDATIONS | 140 |
| 8.3 | FURTHER RESEARCH | 140 |
| REFERENCES | | 142 |

LIST OF FIGURES

| | |
|--|----|
| Figure 2.1 : Eldest and most primitive type water wheel | 5 |
| Figure 2.2 : Overshot water wheel | 6 |
| Figure 2.4: Main characteristic curves for a Kaplan Turbine | 16 |
| Figure 2.5: Constant speed curves | 16 |
| Figure 3.1: Pelton wheel original Patent Document | 19 |
| Figure 3.2: Water flow along a single bucket | 20 |
| Figure 3.3: Basic velocity triangles | 20 |
| Figure 3.4: Schematic diagram of a Pelton runner | 22 |
| Figure 3.5: Spear valve of a Pelton turbine | 23 |
| Figure 3.6: Deflector of a Pelton Turbine | 23 |
| Figure 3.7: Variation of different types of losses with power developed | 24 |
| Figure 3.3: External stroboscopic flow visualization | 28 |
| Figure 3.1: Sediment erosion in Pelton turbine buckets | 30 |
| Figure 4.1: Five Distinct Zones | 34 |
| Figure 4.2: Various pressure tappings | 35 |
| Figure 4.3: Variation of water film thickness | 36 |
| Figure 5.1: Three dimensional view of a bucket | 38 |
| Figure 5.2: Two dimensional view of a jet bucket interaction | 39 |
| Figure 5.3: Illustration on flow through one side of a Pelton bucket | 41 |
| Figure 6.1(b) : Pelton Runner | 48 |
| Figure 6.1(a) : Sectional details of Bucket | 49 |
| Figure 6.1: Pelton runner details | 49 |
| Figure 6.2: Details of the nozzle | 49 |
| Figure 6.3: The test rig | 50 |
| Figure 6.4: Bourdon gauge | 51 |
| Figure 6.5: The Pony brake | 51 |
| Figure 6.6: Force gauge | 52 |
| Figure 6.7: Sieve Shaker | 53 |
| Figure 6.8: Different size of sieves | 54 |
| Figure 6.9 : The Surface roughness tester | 54 |
| Figure 6.10 : Pneumatic grinder | 55 |
| Figure 6.11 : Pneumatic grinder and heads | 55 |
| Figure 6.12: Filling sand to the bucket | 57 |
| Figure 6.13: Removing excess sand after one minute | 57 |
| Figure 6.14: Closer view of Pelton Runner buckets after pasting sand | 58 |
| Figure 6.15: Closer view of Pelton Runner buckets after pasting sand | 58 |
| Figure 6.16: Pelton Runner ready for testing | 59 |
| Figure 6.17: Flow control valve in the experimental setup | 60 |
| Figure 7.1: Nozzle characteristics | 65 |
| Figure 7.2: Variation of brake Load with different spear opening for different roughness heights | 66 |
| Figure 7.3: Variation of brake Load with different spear opening for different roughness heights | 67 |
| Figure 7.4: Variation of Rotational speed for different loads on the runner with different roughness heights in the bucket | 68 |
| Figure 7.5: Variation of power developed by the runner with roughness height in the bucket- Full spear travel | 69 |
| Figure 7.6: Variation of power developed by the runner with roughness height in the bucket- $\frac{3}{4}$ spear travel | 70 |

| | |
|--|-----|
| Figure 7.7: Variation of power developed by the runner with roughness height in the bucket- $\frac{1}{2}$ spear travel | 71 |
| Figure 7.8: Variation of percentage power loss with different roughness conditions in the bucket- Full spear travel | 72 |
| Figure 7.9: Variation of percentage power loss with different roughness conditions in the bucket- $\frac{3}{4}$ spear travel | 73 |
| Figure 7.10: Variation of percentage power loss with different roughness conditions in the bucket- $\frac{1}{2}$ spear travel | 74 |
| Figure 7.11: Variation of percentage power loss with four loads, three spear openings four roughness heights | 75 |
| Figure 7.12: EES program interface for solving mathematical model | 77 |
| Figure 7.13: EES solution window as appear in the software | 78 |
| Figure 7.14: Variation of Two categories of power loss- spear travel - full | 80 |
| Figure 7.15: Variation of Two categories of power loss- $\frac{3}{4}$ Spear Travel | 82 |
| Figure 7.16: Variation of Two categories of power loss- $\frac{1}{2}$ Spear Travel | 84 |
| Figure 7.17: Variation of total predicted percentage power loss for different spear travels | 86 |
| Figure 7.18: Variation of Experimental and Theoretically predicted values of percentage power loss - full spear opening | 88 |
| Figure 7.19: Variation of Experimental and Theoretically predicted values of percentage power loss - $\frac{3}{4}$ spear opening | 89 |
| Figure 7.20: Variation of Experimental and Theoretically predicted values of percentage power loss - $\frac{1}{2}$ spear opening | 91 |
| Figure 7.20: Thickness of the splitter observed through a magnifying glass –front view | 92 |
| Figure 7.21: Thickness of the splitter observe through a magnifying glass – plan view | 93 |
| Figure 7.22 : Replica of a turbine bucket made out from Epifix glue | 94 |
| Figure 7.23 : Replica of a turbine bucket made out from plastoparis | 94 |
| Figure 7.24: Variation of no load speed with spear opening for original runner and roughness height | 99 |
| Figure 7.25: Variation of power developed by the runner with roughness height in the bucket- Full spear travel | 100 |
| Figure 7.26: Variation of power developed by the runner with roughness height in the bucket- Spear opening - $\frac{3}{4}$ | 101 |
| Figure 7.27: Variation of power developed by the runner with roughness height in the bucket- Spear opening - $\frac{1}{2}$ | 102 |
| Figure 7.28: Variation of percentage power loss with load for four roughness heights in the bucket- Spear opening - full | 103 |
| Figure 7.29: Variation of percentage power loss with load for four roughness height in the bucket- Spear opening - $\frac{3}{4}$ | 104 |
| Figure 7.30: Variation of percentage power loss with load for four roughness heights in the bucket- Spear opening - $\frac{1}{2}$ | 105 |
| Figure 7.31: Variation of percentage power loss with load for four roughness heights and three spear openings | 106 |
| Figure 7.32: Variation of percentage power loss due to direct friction and indirect friction for four loads and four roughness heights - Spear opening - full | 108 |
| Figure 7.33: Variation of percentage power loss due to direct friction and indirect friction for four loads and four roughness heights - Spear opening - $\frac{3}{4}$ | 109 |

| | |
|---|-----|
| Figure 7.34: Variation of percentage power loss due to direct friction and indirect friction for four loads and four roughness heights - Spear opening - $\frac{1}{2}$ | 111 |
| Figure 7.35: Variation of predicted total percentage power loss with four loads ,four roughness heights and three spear openings | 112 |
| Figure 7.36: Variation of predicted and experimental percentage power loss for four roughness heights – spear opening – full | 114 |
| Figure 7.37: Variation of predicted and experimental percentage power loss for four roughness heights – spear opening – $\frac{3}{4}$ | 115 |
| Figure 7.38: Variation of predicted and experimental percentage power loss for four roughness heights – spear opening - $\frac{1}{2}$ | 117 |
| Figure 7.39: Variation of power developed by turbine for four loads and three spear openings in two conditions in the splitter. | 119 |
| Figure 7.40: Variation of power developed by turbine for four loads and three spear openings in two conditions in the splitter – roughness height - $106\mu\text{m}$ | 120 |
| Figure 7.41: Variation of power developed by turbine for four loads and three spear openings in two conditions in the splitter – roughness height - $181\mu\text{m}$ | 121 |
| Figure 7.42: Variation of power developed by turbine for four loads and three spear openings in two conditions in the splitter – roughness height - $318\mu\text{m}$ | 122 |
| Figure 7.43: Variation of power developed by turbine for four loads and three spear openings in two conditions in the splitter – roughness height - $512\mu\text{m}$ | 123 |
| Figure 7.44: Variation of percentage power loss due to splitter thickness for original runner and four roughness heights introduced in the buckets for three spear openings | 125 |
| Figure 7.45: flow through turbine bucket with sharp splitter | 126 |
| Figure 7.46: flow through turbine bucket with blunt splitter | 126 |
| Figure 7.47: impact of jet on a flat plate | 127 |
| Figure 7.48: area of water jet disturbed by splitter | 127 |
| Figure 7.49 : Variation of experimental and predicted total percentage power loss with four roughness heights – spear opening - full | 129 |
| Figure 7.50: Variation of experimental and predicted total percentage power loss with four roughness heights – spear opening - $\frac{3}{4}$ | 131 |
| Figure 7.51: Variation of experimental and predicted total percentage power loss with four roughness heights – spear opening - $\frac{1}{2}$ | 133 |
| Figure 7.52: Spillway Effect | 134 |
| Figure 7.52: Coanda effect | 136 |

LIST OF TABLES

| | |
|---|-----|
| Table 3.1: Features of each flow regime | 27 |
| Table 7.2: Brake load for different roughnesses and spear travels | 65 |
| Table 7.3: No load speed for different roughnesses and spear travel | 66 |
| Table 7.4: Rotational speed for different loads on the runner and different roughness heights | 67 |
| Table 7.5: Power developed by the turbine with various surface roughness conditions | 68 |
| Table 7.6: Power developed by the turbine with various surface roughness conditions | 69 |
| Table 7.7: Power developed by the turbine with various surface roughness conditions | 70 |
| Table 7.8: Percentage Power loss in the turbine with various surface roughness conditions | 71 |
| Table 7.9: Percentage Power loss in the turbine with various surface roughness conditions | 72 |
| Table 7.10: Percentage Power loss in the turbine with various surface roughness conditions | 73 |
| Table 7.11: Percentage power loss in the turbine for three spear openings and roughness heights | 74 |
| Table 7.12: Percentage power loss due to indirect friction and direct friction | 79 |
| Table 7.13: Percentage power loss due to indirect friction and direct friction | 81 |
| Table 7.14: Percentage power loss due to indirect friction and direct friction | 83 |
| Table 7.15: Total percentage power loss for three spear openings | 85 |
| Table 7.16: Predicted and experimental values of percentage power losses for roughness conditions in the bucket - spear opening - full | 87 |
| Table 7.17: Predicted and experimental values of percentage power losses for roughness conditions in the bucket - spear opening - $\frac{3}{4}$ | 88 |
| Table 7.18: Predicted and experimental values of percentage power losses for roughness conditions in the bucket - spear opening - $\frac{1}{2}$ | 90 |
| Table 7.19: Results of Experiment No 2 | 95 |
| Table 7.20: No load speed for different roughnesses and spear travel | 98 |
| Table 7.21: Power developed by the turbine with various surface roughness conditions - Spear opening - Full | 99 |
| Table 7.22: Power developed by the turbine with various surface roughness conditions - Spear Opening - $\frac{3}{4}$ | 100 |
| Table 7.23: Power developed by the turbine with various surface roughness conditions | 101 |
| Table 7.24: Percentage Power loss in the turbine with various surface roughness conditions for full spear opening | 102 |
| Table 7.25: Percentage Power loss in the turbine with various surface roughness conditions | 103 |
| Table 7.26: Percentage Power loss in the turbine with various surface roughness conditions Spear opening - $\frac{1}{2}$ | 104 |
| Table 7.27: Experimental values of percentage power loss for three spear openings | 105 |
| Table 7.28: predicted percentage power loss due to direct effect of friction and indirect effect of friction | 107 |
| Table 7.29 : predicted percentage power loss due to direct effect of friction and indirect effect of friction | 108 |

| | |
|--|-----|
| Table 7.30: predicted percentage power loss due to direct effect of friction and indirect effect of friction | 110 |
| Table 7.31: predicted total percentage power loss for three spear openings and four roughness heights | 111 |
| Table 7.32 : predicted and experimental values of percentage power loss for four roughness heights | 113 |
| Table 7.33: predicted and experimental values of percentage power loss for four roughness heights | 114 |
| Table 7.34: predicted and experimental values of percentage power loss for four roughness heights | 116 |
| Table 7.35: power developed by original runner for sharp splitter and blunt splitter for three spear openings | 118 |
| Table 7.36: power developed by turbine for sharp splitter and blunt splitter for three spear openings – roughness height -106 μ m..... | 119 |
| Table 7.37: power developed by turbine for sharp splitter and blunt splitter for three spear openings – roughness height -181 μ m..... | 120 |
| Table 7.38: power developed by turbine for sharp splitter and blunt splitter for three spear openings – roughness height -318 μ m..... | 121 |
| Table 7.39: power developed by turbine for sharp splitter and blunt splitter for three spear openings – roughness height -512 μ m..... | 122 |
| Table 7.40: percentage power loss due to the splitter thickness for four roughness heights and for three spear openings | 124 |
| Table 7.41: Predicted percentage power loss due to the splitter thickness and total predicted loss four roughness heights | 128 |
| Table 7.42: Predicted percentage power loss due to the splitter thickness and total predicted loss four roughness heights | 130 |
| Table 7.43: Predicted percentage power loss due to the splitter thickness and total predicted loss four roughness heights | 132 |

NOTATION

| | |
|-----------|--|
| c_f | Coefficient of friction |
| D | Diameter of the jet |
| D_h | Hydraulic diameter |
| F_{co} | Coriolis force |
| F_{ct} | Centrifugal force |
| h | Thickness of the flow sheet |
| H | Water head |
| l | Width of the flow sheet |
| L | Total distance of the flow path |
| l_1 | Width of the flow sheet at the inlet |
| l_2 | Width of the flow sheet at the outlet |
| P_b | Over pressure on the bucket |
| P_{co} | Power dissipated due to coriolis force |
| P_{ct} | Power dissipated due to Centrifugal force |
| P_f | Power dissipated due to direct friction |
| P_{in} | Power loss due to indirect effect of friction |
| P_p | Power dissipated due to pressure variation |
| P_1 | Total power developed by the turbine |
| P_2 | Power developed |
| r | Radius of the bucket |
| R | Mean radius of the runner |
| t | Thickness of the splitter |
| U | Velocity of the flow in the nozzle |
| U_1 | Velocity of the Pelton runner |
| V | Relative velocity of water |
| v_1 | Absolute velocity of water at the entrance to the bucket |
| V_1 | Relative velocity of water at the entrance to the bucket |
| v_2 | Absolute velocity of water at the exit from the bucket |
| V_2 | Relative velocity of water at the exit from the bucket |
| $v_{f,o}$ | velocity of flow at outlet |

| | |
|----------------|---------------------------------------|
| $v_{w,o}$ | velocity of whirl at outlet |
| $v_{f,i}$ | velocity of flow at inlet |
| $v_{w,i}$ | velocity of whirl at inlet |
| x | Distance measured along the flow path |
| β | Blade angle |
| δ | Boundary layer theory |
| δ^* | Displacement thickness |
| θ | Momentum thickness |
| τ_0 | Shear stress |
| \dot{m} | Mass flow rate |
| \dot{m}_{sp} | Mass flow rate hit the splitter |



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